Determination of the electric field in highly-irradiated silicon sensors using edge-TCT measurements

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Motivation

- Modelling the electric field for heavily irradiated n⁺-p sensors
 - input to simulations
 - understanding the radiation damage at high fluences
 - where does the "standard" device model break down?
- Conventional-TCT which was used to extract the electric field shape at low fluences from the time evolution of the induced currents is not possible too much trapping.
 But Edge-TCT (*IEEE Trans. Nucl. Sci. Vol. 57(4), 2010, p. 2294*) can …
- It aims to develop a method allowing accurate extraction of measurements. It should be easily fed to the simulators and should serve to understand also the fundamental reasons for the change.

Samples and measurement technique

ATLAS 07 mini-strip sensors (single p-stop+p-spray isolation)

Thickness	Crystal	pitch	<i>n</i> ⁺ width	Strip length	Area	B-doping	U_{fd}
μm	orientation	μm	μm	cm	cm^2	cm^{-3}	V
300	$\langle 100 \rangle$	100	20	0.8	0.62	2.8×10^{12}	180

- Samples irradiated with reactor neutrons to 1,2,5,10e15 cm⁻² and 200 MeV pions to 1.5e15 cm⁻²
- Samples were irradiated for 80min @ 60°C
- Samples were measured at -20°C and measured in forward and reverse direction with Edge-TCT (neighbors at the same potential as the strips)





Measurement of velocity profiles



$$x \xleftarrow{p} \xrightarrow{p} n^{+} \uparrow$$

$$e \xrightarrow{y_{0}} p^{+} \downarrow$$

$$E \xrightarrow{h} \xrightarrow{p-type} p^{+} \downarrow$$

$$I(y,t \sim 0) \approx \frac{Ae_0 N_{e,h}}{W} \left[\overline{v}_e(y) + \overline{v}_h(y) \right] \quad , \quad t \ll \tau_{eff,e,h}$$

The trapping can be completely taken out of the equation! (The major obstacle of extraction of physics parameters from time evolution in conventional/Top-TCT is severe trapping)

Different methods were tried in [200,t_{int}]

- integral
- value at different times
- slope of the current pulse rise

Comparable results for all - no big difference between them

Correctness of the above equation depends on several assumptions:

- attenuation of the laser should be small over the distance of several strips – effective weighting field
- implant width/strip pitch should be as close to 1 as possible – effecting the drift paths and effective weighting field
- trapping is much longer than the rise time

Effect of strip proximity/surface



- the surface condition (humidity/temperature, salts, impurities on the surface influence the electric field)
- assumption of electric field with only E_{ν} component can be too simplistic
- as this conditions can change with time/temperature/humidity it is difficult to know them
- in the analysis of the data this effects can be probed/evaluated by changing the start of first (modeling)

Effect of finite attenuation length

- Induction from the neighbors is affected by the attenuation (follows from symmetry)
- Simulation of 6 neighbors was used to check the influence on effective weighting field





$$\overrightarrow{E_w} = \frac{1}{p} \int \overrightarrow{E_w}(\vec{r}) \exp(-\lambda_{abs} \cdot x) \, dx$$
$$R_y = \frac{E_w(\lambda_{abs})}{E_w(\lambda_{abs} \to \infty)}$$

- For 6 strips the difference in Ew<10% (the more strips are bonded the better)
- Only for $\lambda_{abs} \rightarrow \infty$ the $E_w(\lambda_{abs})$ sums from all contributions yield effectively weighting field of the Ew=(0,1/W,0)
- Simulation of 6 neighbors (von Neuman boundary condition worst case) was used to check the deviation from Ew=(0,1/W,0)



Modeling-extraction of the Efield



Step in y was 5 μm defining N_F points in which field E_k is calculated (free parameters of the fit)

 σ_{vel} - relative uncertainty of velocities ~ 2% w_{pen} - dumps large fluctuations of the field

 $\int_0^d E(y) \, \mathrm{d}y = U$

Electric field in non-irradiated detector



- very good agreement of the model (solid lines) with data points (shifted by 0.1 for clearer view)
- extracted electric field is in reasonable agreement with the electric field in pad detector with uniform doping



vscale parameter is a function of voltage, due to: finite rise time of intial current an

shows the voltage dependence of *vscale(U)*, with which the signal from the model calculation has to be multiplied in order to describe the velocity profiles. It has to be introduced, as the relation between the initial slope of the pulse, which is used to determine the velocity profiles, and the actual velocities of the charge carriers, is not known with sufficient accuracy. An increase of vscale with decreasing *U* is expected from the finite rise time tr. of the initial current transient

Influence of electronics and carrier lifetimes

Forward bias 2.2×10 • • • U = 25 V 2×10⁴





y [µm]



у [µm]



U = 25 V • • • U = 50 V

• • • U = 75 V

+ + + U = 100 V

150 *у* [µm] 200

250

300

100

0

50

6×10

3×10



Reverse bias





Effective doping concentration



Double junction with symetrical

Pion irradiated samples



Conclusions