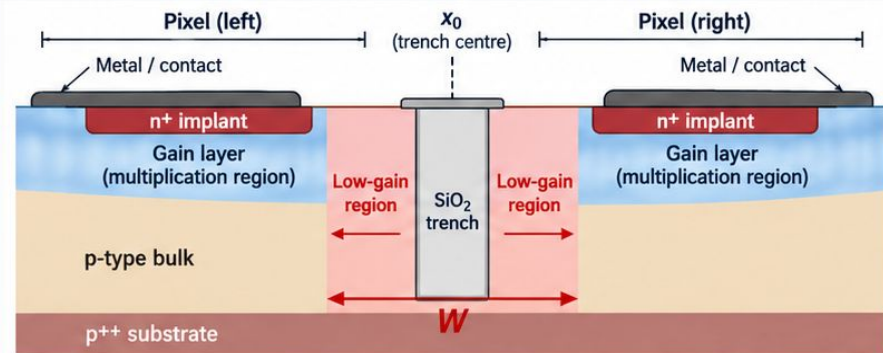


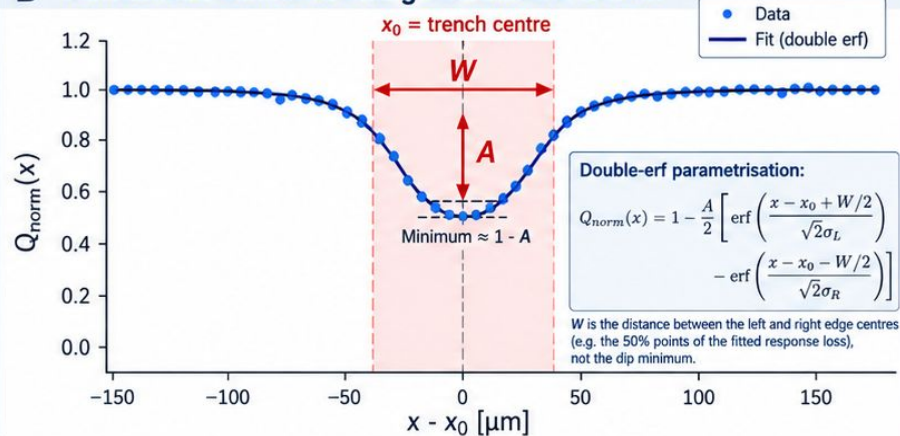
Conceptual parametrisation of TI-LGAD trench response

A TI-LGAD cross-section (two neighbouring pixels)

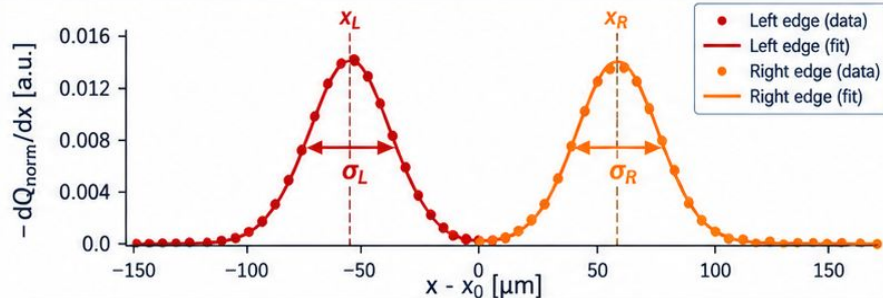


W is not the physical etched trench width only,
but the effective response-loss width extracted from the signal profile.

B Normalised collected charge across the trench

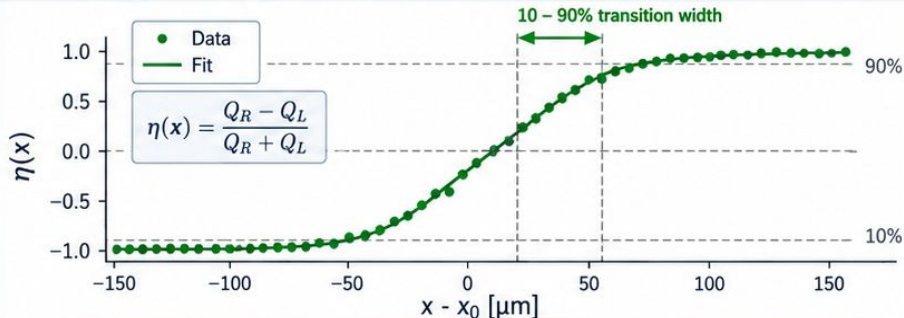


C Edge response and extraction of σ



σ_L and σ_R quantify edge broadening / transition sharpness;
they are extracted from the fitted left and right edges, even when the central response shows a dip.

D Charge-sharing across the trench



η provides an independent charge-sharing observable complementary to $Q_{\text{norm}}(x)$.

Parameter summary

x_0 : trench centre from the fit / symmetry point

W : effective trench-affected width

A : relative charge-loss amplitude

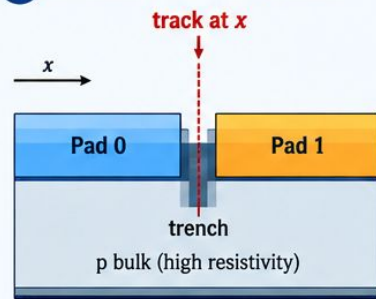
σ_L, σ_R : edge-transition widths

$\eta(x)$: charge-sharing observable

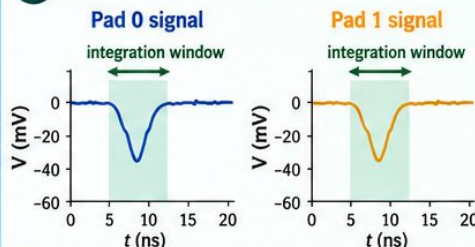
Applicable to both test beam and TCT scans

A From detector signals to normalised total response

1 Geometry and track position



2 Signals from both pads



$$Q_L(x) = \int_{t_1}^{t_2} V_L(t) dt$$

$$Q_R(x) = \int_{t_1}^{t_2} V_R(t) dt$$

3 Normalisation and total response

Each pad is normalised to its own bulk response (far from the trench):

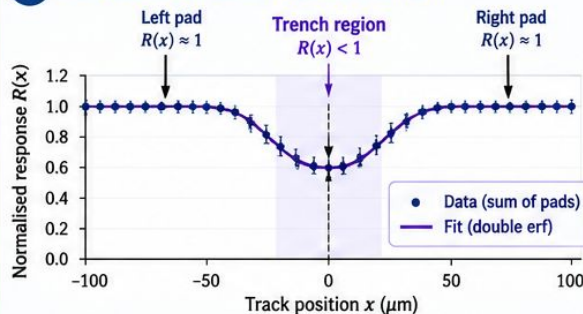
$$q_L(x) = \frac{Q_L(x)}{Q_{L,bulk}}$$

$$q_R(x) = \frac{Q_R(x)}{Q_{R,bulk}}$$

Total (charge-sharing independent) normalised response:

$$R(x) = q_L(x) + q_R(x)$$

4 Measured behaviour (typical example)



Response deficit:

$$D(x) = 1 - R(x)$$

- $R(x) \approx 1$ away from trench (full response)
- Dip at trench due to incomplete charge collection
- Charge sharing alone would give $R(x) \approx 1$ (no dip)

B Parametrisation with a double error function

1 Fitting function

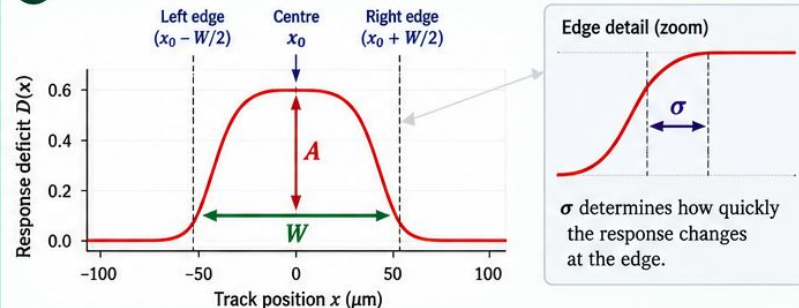
The response deficit $D(x)$ is described by a double error function:

$$D(x) = 1 - R(x) = \frac{A}{2} \left[\text{erf} \left(\frac{x - (x_0 - W/2)}{\sqrt{2}\sigma} \right) - \text{erf} \left(\frac{x - (x_0 + W/2)}{\sqrt{2}\sigma} \right) \right]$$

2 Meaning of the parameters

- x_0 – centre of the response deficit (trench position)
- A – depth of the response deficit (maximum loss, $0 \leq A \leq 1$)
- W – effective width of the affected region (distance between midpoints)
- σ – transition sharpness (controls the edge slope)

3 Visual meaning of W and σ



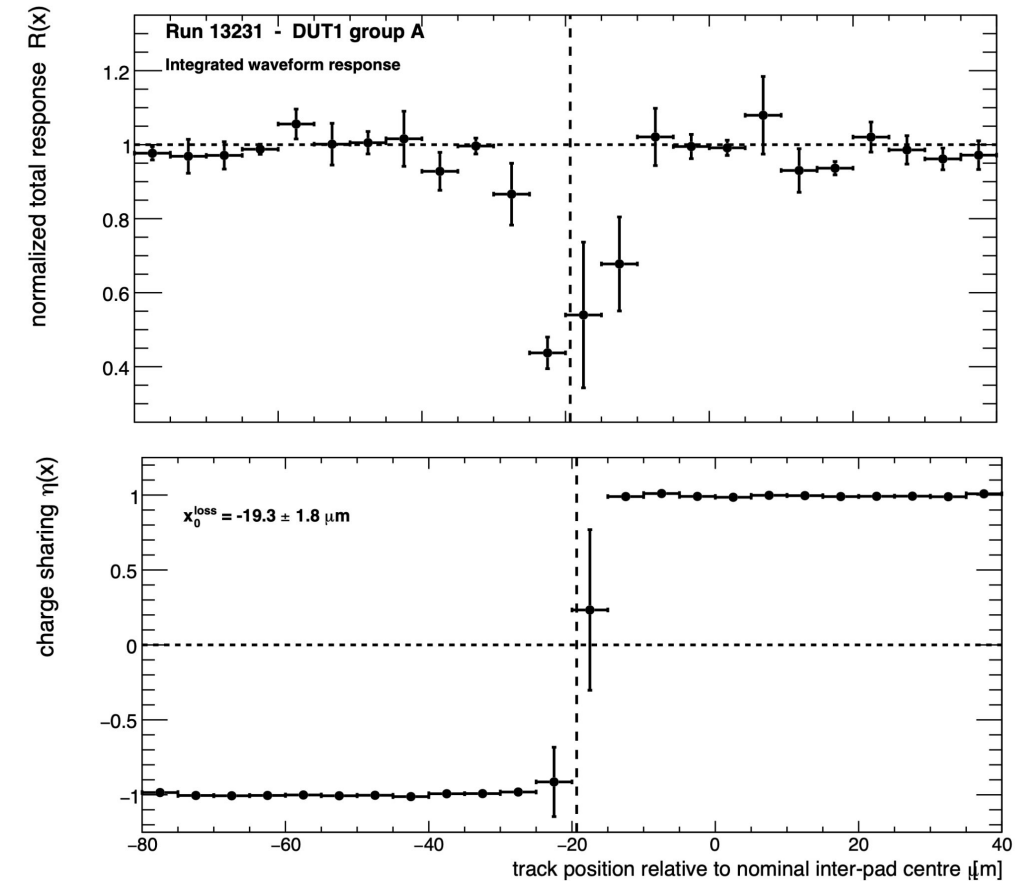
4 Figure of merit

Integrated response loss (area of the deficit):

$$F = A \cdot W$$

- Single, design-independent number
- Quantifies the overall impact of the trench
- Can be compared across different TI-LGAD designs

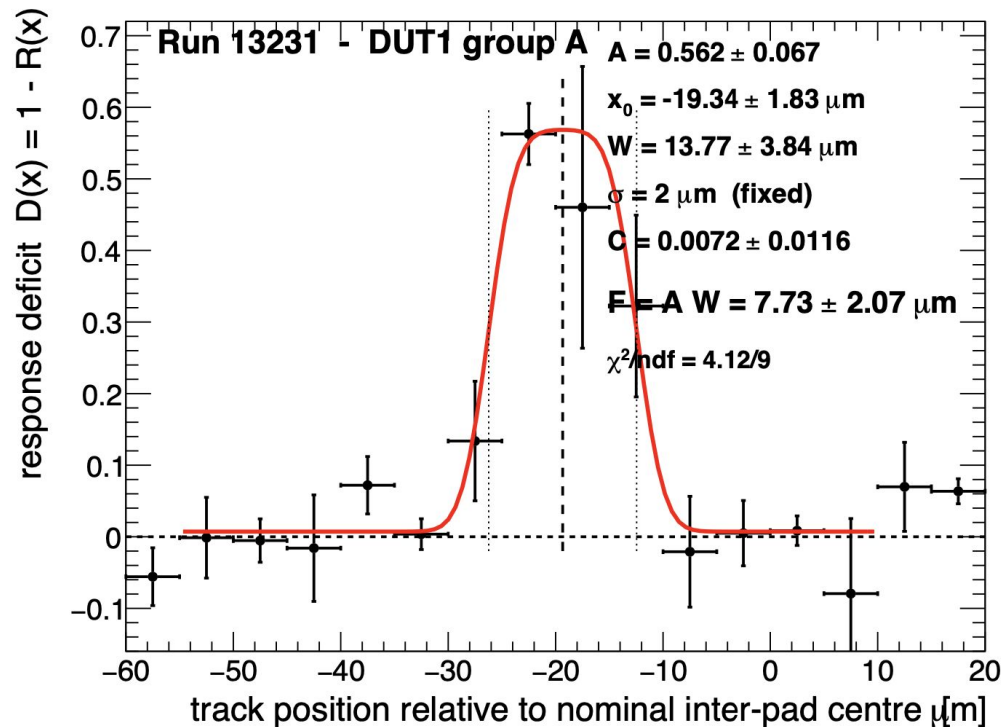
Testing the concept for wafer 5 (I)



$$r_L(x) = \frac{S_L(x)}{S_{L,\text{bulk}}}, \quad r_R(x) = \frac{S_R(x)}{S_{R,\text{bulk}}},$$
$$R(x) = r_L(x) + r_R(x)$$
$$\eta(x) = \frac{r_R(x) - r_L(x)}{r_R(x) + r_L(x)}$$

I normalize the integrated charge of each pad to its own bulk response. The sum $R(x)$ tells me whether charge is actually lost, while $\eta(x)$ tells me how the charge moves from one pad to the other.

Testing the concept for wafer 5 (II)



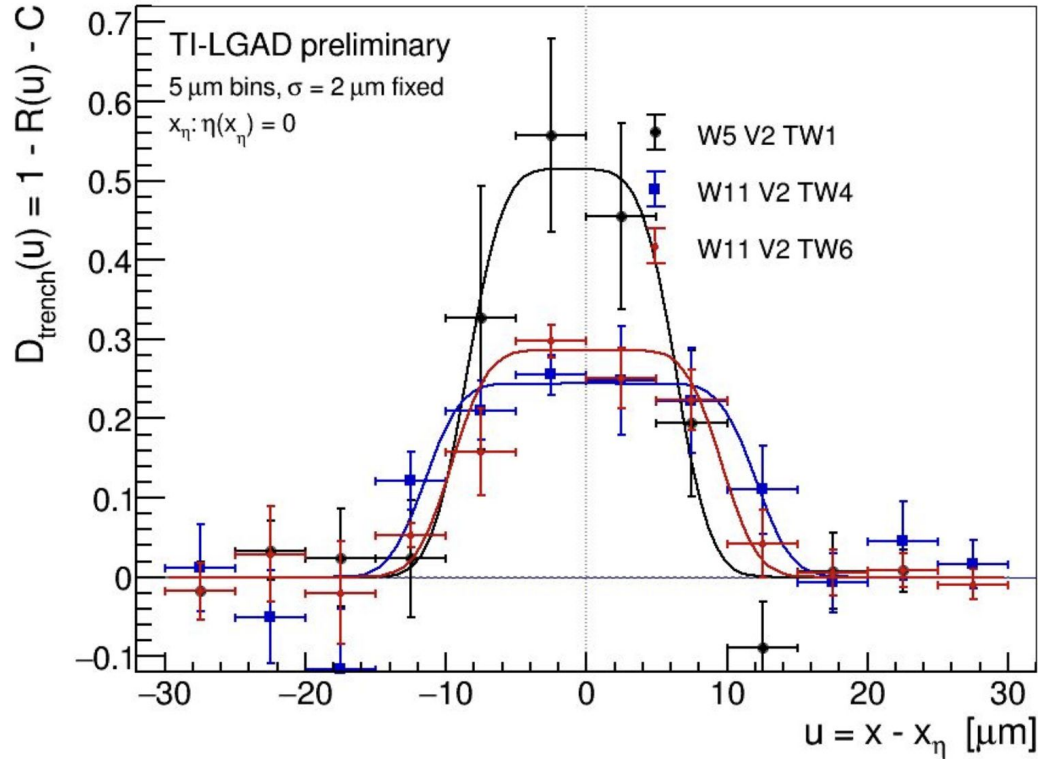
The baseline is consistent with zero, so this is a localized response deficit.

The fitted centre is $x_0 = -19.3 \mu\text{m}$, while the completely independent charge-sharing transition is around $-19.7 \mu\text{m}$

When I change the assumed edge smearing, A and W change substantially because they are correlated. But their product AW remains much more stable.

The double-erf fit gives $F = 7.73 \mu\text{m}$, while directly integrating the measured response deficit gives about $7.8 \mu\text{m}$. The agreement shows that AW is measuring the integrated response loss, rather than just being an arbitrary combination of fit parameters

Standardised TI-LGAD response-loss comparison



Common procedure

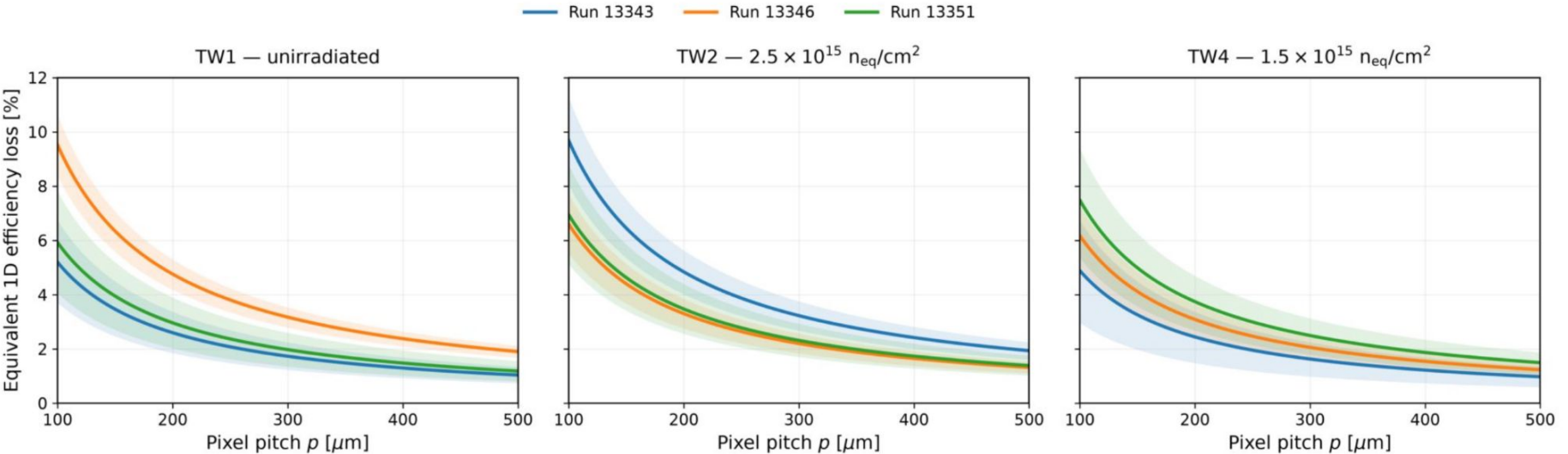
- Align each structure to the charge-sharing transition x_η :
 $\eta(x_\eta) = 0 \quad u = x - x_\eta$
- Same analysis for all structures: 5 μm bins, $|u| < 30 \mu\text{m}$ $\sigma = 2 \mu\text{m}$
- The fitted response-loss centres are consistent with the charge-sharing centre:
 $u_0 \approx 0$

$$F = AW = \int D_{\text{trench}}(u) du$$

$$\begin{aligned} \text{W5 TW1} &: 7.66 \pm 1.92 \mu\text{m} \\ \text{W11 TW4} &: 5.85 \pm 1.13 \mu\text{m} \\ \text{W11 TW6} &: 5.42 \pm 0.66 \mu\text{m} \end{aligned}$$

The fitted $F=AW$ values are consistent with direct numerical integration, supporting F as a candidate common response-loss metric for TI-LGAD designs.

Equivalent inter-pixel efficiency loss vs pixel pitch



% on the y-axis is the estimated fraction of efficiency we lose because of the inter-pixel region

From measured inter-pixel efficiency to pitch impact

1 Measure $\epsilon(u)$

Use the two-pixel efficiency profile across the inter-pixel boundary. The local reference efficiency comes from nearby sidebands.

$$\epsilon(u) / \epsilon_{\text{local}}$$



2 Integrate deficit

Convert the efficiency dip into an equivalent fully inefficient width.

$$w_{\text{eff}}^{\epsilon} = \int [1 - \epsilon(u)/\epsilon_{\text{local}}] du$$



3 Scale to pitch

For one inter-pixel boundary per pitch, the equivalent 1D average loss is the effective width divided by the pitch.

$$L_{\epsilon}(p) = w_{\text{eff}}^{\epsilon} / p$$

Interpretation

$w_{\text{eff}}^{\epsilon}$ is the width of an ideal zero-efficiency strip that would give the same integrated loss as the measured inter-pixel profile.

Quick numerical intuition

If $w_{\text{eff}}^{\epsilon} = 5 \mu\text{m}$: 5% at $p = 100 \mu\text{m}$ •
2.5% at $200 \mu\text{m}$ • 1% at $500 \mu\text{m}$

Extending the TI-LGAD parametrization to timing

